

Characteristics of Thermal Neutron Flux Distribution in a Phantom Irradiated by Epithermal Neutron Beam from Double Layer Beam Shaping Assembly (DBSA)

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Abstract. A simulation study on the Double-layer Beam Shaping Assembly (DBSA) system has been carried out. This study used fast neutron beam resulting from reactions of 30 MeV protons with beryllium target. The MCNPX code was utilized to design the DBSA and the phantom as well as to calculate neutron flux on the phantom. The distribution of epithermal neutron flux and gamma in the DBSA and phantom were computed using the PHITS code. The spectrum of radiation beams generated by the DBSA shows the characteristics that the typical epithermal neutron flux of 1.0×10^9 n/(cm².s), the ratio of epithermal to the thermal and fast neutron flux of 344 and 85, respectively and the ratio of gamma dose to the epithermal neutron flux of 1.82×10^{-13} Gy.cm². The test of epithermal neutron beams irradiation on the water phantom shows that epithermal neutrons are thermalized and penetrate the phantom up to 12 cm in depth. The maximum value of neutron flux is 1.1×10^9 n/(cm².s) at a depth of 2 cm in phantom.

Keywords: double-layers BSA, MCNPX, PHITS, neutron flux, phantom

Introduction

The Boron Neutron Capture Therapy (BNCT) is a promising therapeutic method for cancer treatment owing to its capability of killing cancer cells selectively with the use of ¹⁰B compounds in the cell, irradiated by neutrons. Interactions of the neutron with ¹⁰B nucleus produce α -particle and ⁷Li nucleus through ¹⁰B(n, α)⁷Li reaction. It is the energy of α particle that is utilized to destroy cancer cells in body tissues. The range of α -particles is short, within the size of a cell, allowing radiation effect to be focused entirely on the cancer cell and suppressing negative effects on healthy cells (Sauerwein *et al.*, 2012). Therapies for shallow cancer are carried out with thermal neutrons while for deeper cancer with epithermal neutrons (Tanaka *et al.*, 2011).

A neutron source currently being developed is the accelerator. An accelerator is a more feasible neutron source because of its possibility to be built close to a hospital (Kreiner *et al.*, 2016). Cyclotron type accelerators are widely developed in various countries such as Japan, specifically the KURI Institute, which

develops the C-BENS and Korea, which develops a BNCT based accelerator (AB-BNCT) (Lai and Sheu, 2017). Both types of cyclotrons use protons with 30 MeV of energy. One part of the cyclotron that is still in development is Beam Shaping Assembly (BSA). The BSA is a system that transforms fast neutrons into epithermal neutrons while also suppresses ensuing contaminants (Avagyan *et al.*, 2017; Monshizadeh *et al.*, 2015).

BSA designs used in neutron sources typically consist of a moderator, filter, reflector, and collimator as their main components (Kasesaz *et al.*, 2014). Each of the components is commonly designed with single layer configuration, i.e., they only use one type of material. The disadvantage of the single layer configuration is that every component does not work efficiently, causing moderated fast neutrons not being transformed into epithermal neutrons with such quality and intensity that agree with the requirements of BNCT therapies. To overcome this weakness, double layer, even multilayer, configurations may be developed.

The double-layer configuration BSA or DBSA is introduced. It is expected to produce neutron beams with

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better intensity and quality from the evidence that combining two suitable materials yields better quality. Using two-layered moderators combination, Dao-wen *et al.* (2012) were able to improve moderation up to 19.3%. Adib *et al.* (2016) combined two or more filter materials and succeeded to produce epithermal neutron beams within a range of 1.5 to 10 keV. Better results were also obtained when two reflectors were combined. A combination of reflector materials such as tungsten (W) and molybdenum (Mo) can multiply neutron reflection to five times as compared to when only tungsten is used (Asnal *et al.*, 2015, Kasesaz *et al.*, 2013).

In order to find the characteristics of BSA that consist of components made of two different materials, quality tests are required on the beams generated by the BSA (Monshizadeh *et al.*, 2015; Kasesaz *et al.*, 2013; Tanaka *et al.*, 2011). In principle, there are two ways to know the quality of beams for BNCT, (a) that are by assessing their quality in the air and (b) in a water phantom. Assessment of radiation beams in the air is an assessment that complies the IAEA-TECDOC-1223 (2001). As for the assessment in the water phantom, it is emphasized on the ability of radiation beams to penetrate the phantom and the dose of neutron sustained by a tumor (Ghal-Eh *et al.*, 2017). Water phantom is typically chosen as a testing material because 70% of a human body consists of water (Tsukamoto *et al.*, 2011).

This article reports characteristics of radiation beams produced by DBSA and their penetration quality in the water phantom. We plan to design the DBSA combining two cheaper materials that are available in the market while maintaining good moderation, reflection, and filtering quality. If this new design of the DBSA proves successful, then the design would be implemented to the BNCT that is currently developed in Indonesia.

Materials and Methods

In this simulation study, the neutron source is from the interaction of proton (30 MeV, $I = 1$ mA) with ^9Be target through $^9\text{Be}(p,n)^9\text{B}$ reactions (Hashimoto *et al.*, 2014). The neutron beams are assumed to be isotropic and monoenergetic when they are radiated from the target. It is also assumed that the neutrons radiated from the target are fast neutrons, with energy of 28 MeV and neutron yields $\leq 10^{14}$ n/s (Tanaka *et al.*, 2011). Utilizing 30 MeV protons is more advantageous on account of its ability to produce higher neutron flux than low-energy neutron sources. To lower the energy of fast neutrons, turning them into epithermal neutrons, a

Double-layer Beam Shaping Assembly (DBSA) is used. The configuration of the DBSA is shown in Fig. 1.

Materials for DBSA components are selected regarding their corresponding functions and considering their cross-section and availability in the market. The materials used as the moderator in the design of BSA are aluminum (Al) and fluorine (F). The primary reason for the selection of Al and F is their high scattering cross-section. Aluminum has a high cross-section at energies above 10 keV and 25 keV in fluorine (Zaidi *et al.*, 2017; Turkmen *et al.*, 2017).

The materials for reflector are Pb and FeC. They have high density and ability to scatter fast neutron extremely well (Sato *et al.*, 2013). C (graphite) is also used as a reflector for its low cost. Apart from being cheap it also has high scattering cross-section and low absorption, particularly at energies above 1 MeV (Turkmen *et al.*, 2017).

The collimator component under considerations is made of Ni and borated polyethylene materials. Ni is considered to be a stable element when it interacts with neutrons. Some of its isotopes have a short half-life and thus safe to be used as a collimator.

For fast neutron filter, Fe materials are used. The effectiveness of Fe as a high energy neutron filter owes to the ability of Fe to inelastically scatter high energy neutrons passing through Fe. Fe materials are deemed superior in filtering fast neutrons. The ability of Fe to filter fast neutrons derives from its resonant cross-section which is above 10 keV (Ivakin *et al.*, 2011). Thermal neutrons are filtered using a material with high

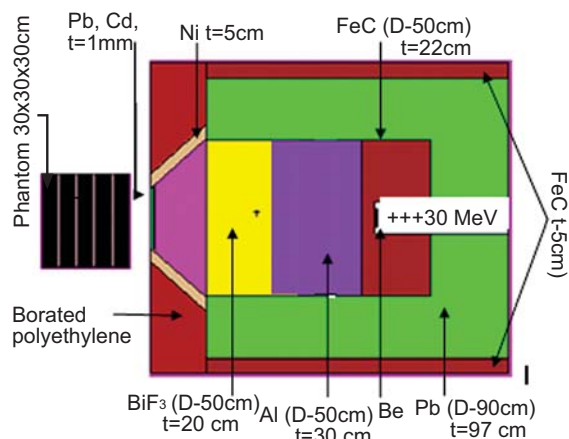


Fig. 1. Model of DBSA and water phantom.

atomic number. Among atoms with high thermal neutrons absorption cross-section is Cd which is frequently used as a thermal neutron filter. A cross-section of 20.600 barn is reasonably effective to absorb thermal neutrons (Osawa *et al.*, 2017; Asnal *et al.*, 2015).

The material for shielding is Pb. It has a relatively constant attenuation coefficient, i.e., $0.05 \text{ cm}^2/\text{g}$ to able to absorb gamma rays with energies of 1-10 MeV (Turkmen *et al.*, 2017). Pb materials are better still as gamma shielding compared to Bi. That is because during its interaction with neutrons, Bi produces a toxic and transforms into ^{210}Pb .

The BSA model being developed as high energy neutron beam processor uses a model of double layer having moderator, reflector, collimator and filter as its primary component, and neutron beam channel that is cylindrical and conical in shape. The model of proton channel in the BSA is in form of a cylinder coated by Pb material. The function of Pb coating as proton reflector is to keep proton from spreading and maintain its focus into the target (Khorshidi, 2017; Hasimoto *et al.*, 2015; Tanaka *et al.*, 2011)

Epithermal neutrons leaving the DBSA are subsequently imposed on water phantom, shaped as $30 \text{ cm} \times 30 \text{ cm} \times 30 \text{ cm}$ box, which is placed 1 cm at the front of the DBSA. In order to determine the change in epithermal neutron flux into thermal neutrons in phantom, a $1 \times 1 \times 1 \text{ cm}$ detector cell was placed in the phantom. The distance between the detectors and each other is 1 cm. The composition of the water phantom is 11.2% of H atoms and 88.8% of O atoms, with the density of 1000 kg/cm^3 (Kreiner *et al.*, 2016; Raaijmakers *et al.*, 2000).

The software used in designing and analyzing particle transports in the DBSA is the Monte Carlo method. Two codes that are used are MCNP and PHITS. Both softwares are widely used in the field of nuclear reactor physics, accelerator design, medical physics (Solovyev *et al.*, 2015; Sato *et al.*, 2013).

In designing the DBSA, the Monte Carlo N particle X (MCNPX) 2.7 code is used (Pelowitz, 2005). The code is run with particle history of 10^6 and multiplication factor of $6.25 \times 10^{15} \text{ n/s}$, in n p h Mode and tally F5 for calculations of important parameters, i.e. thermal neutron beams, epithermal neutron beams, fast neutrons, and gamma dose. Tally DE and DF are used to change fluxes into doses. The corresponding microscopic cross section data is used for simulation by using the ENDF/B-VII and Visual Editor to visualize the geometry of the

MCNPX input. NPS is set to million for each run to ensure the tally results to meet requirement of 10% uncertainty in statistics.

The distributions of neutron and gamma flux in the DBSA and phantom are computed using the Particle and Heavy Ion Transport System (PHITS) code. (Sato *et al.*, 2013). PHITS is also used to determine the spectrum of outgoing neutron-flux on the aperture surface. The track length tally is used in the PHITS calculation. To draw the particle track and visualization geometry of DBSA, the ANGEL software is used. The transport is based on the cross-section data library JENDL-4.0 for neutron and photon, and intra-nuclear cascade (INCL4.6) for proton.

Results and Discussion

Characteristics of epithermal neutron beams from DBSA. Figure 1 shows DBSA as a system processing fast neutrons into epithermal neutrons and suppressing contaminants. DBSA has four main components, those are moderator, reflector, collimator, and filter. Each of the components is formed by a combination of two materials. The moderator is formed of Al and BiF_3 materials, particularly by combining materials with small and large Z. Such combinations are expected to moderate high neutron energy effectively and gradually (Mozhayev *et al.*, 2016). The reflector is formed of a combination of Pb and FeC. Pb functions reflect neutron beams back into the moderator. Pb materials possess good reflectivity property, owing to its large scattering cross section and low absorption cross section fast neutron (Takata *et al.*, 2010). The collimator is formed of a combination of Ni and borated polyethylene, and the filter is formed of a combination of FeC and Cd materials. Fe is used as the filter for fast neutrons and Cd as a thermal neutron filter. The use of two materials on every component of DBSA is intended to enhance the contribution of each material.

Figure 2 shows the distribution of epithermal neutron in the DBSA. Epithermal neutrons resulted from the moderation of fast neutrons produced from interactions of 30 MeV protons with beryllium target (Hashimoto *et al.*, 2015). Highest epithermal neutron fluxes are distributed around FeC filter and AL and BiF_3 moderator. Epithermal neutron flux in the vicinity of moderator and filter reaches $10^{11} \text{ n}/(\text{cm}^2.\text{s})$. The ability of the moderator in moderating fast neutrons into epithermal neutrons is accounted for by fluorine (F) in the BiF_3 material and aluminum (Al) as constituting components

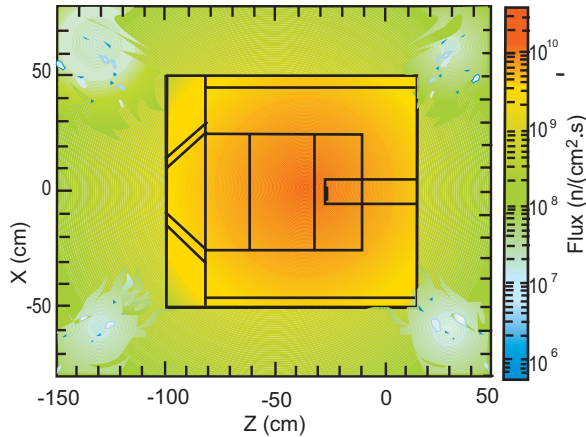


Fig. 2. Distribution of epithermal neutron flux in the DBSA.

of the moderator. The effectiveness of Al and BiF₃ in producing epithermal neutron flux is due to Al that has high scattering cross section to energies of above 10 keV (Ivakhin *et al.*, 2011). Interactions between neutrons and Al material produce epithermal neutrons through ²⁷Al (n,2n)²⁷Al reactions (Ma *et al.*, 2017). With regard to the contribution of BiF₃ in moderating fast neutrons, it is because of the presence of fluorine (F) in the BiF₃ material. Fluorine is an element that has such high scattering cross section to fast neutrons that BiF₃ material also contributes to increasing the number of epithermal neutrons and reducing the number of thermal neutrons. Lastly, Bi contributes to reducing gamma radiations (Fantidis and Nicolaou, 2018).

The quality of increasing epithermal neutrons is also sustained by the presence of the FeC filter placed in front of the moderator as a filter to high energy neutrons. The effectiveness of FeC as a high-energy neutron filter is attributed to the ability of FeC to in-elastically scatter high energy neutrons that pass through FeC material. Fe Material with 4 cm thickness is adequately effective in reducing the energy of the order of MeV into that of an epithermal neutron (Asnal *et al.*, 2015). Figure 3 shows the spectrum of neutron flux produced by the DBSA calculated at the location of the aperture. The spectrum has a peak at the energy of 10 keV with maximum epithermal neutron flux of 1.0×10^9 n/(cm².s). Another researcher also found a similar value of epithermal neutron flux (Mitsumoto *et al.*, 2010). Simulation results using the MCNPX code obtained the following characteristics of neutron beams: the epithermal flux of 1.0×10^9 n/(cm².s), a ratio of epithermal to thermal and fast neutron of 344 and 85, and a ratio

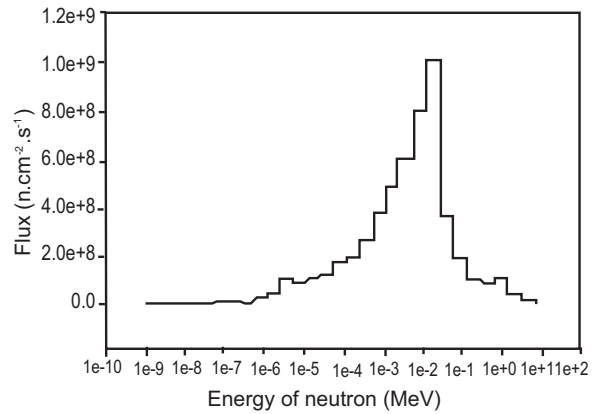


Fig. 3. Spectrum of the neutron flux at the end of DBSA.

of gamma-neutron dose to an epithermal neutron flux of 1.82×10^{-13} Gy. cm².

Characteristics of neutron and gamma beams in water phantom. Fig. 4 shows the distribution of the epithermal neutron in the DBSA and the phantom. Epithermal neutrons that enter the phantom continually decrease in energy (depicted by changes in colour from yellow to blue in the phantom). The decrease in epithermal neutron flux is due to epithermal neutrons transforming into thermal neutrons during interactions with hydrogen atoms. This process is called thermalization (Hignett *et al.*, 2002).

The neutron flux outside the DBSA, particularly outside the collimator decreases significantly. Based on the evaluation at 35 cm outside of the aperture, the neutron

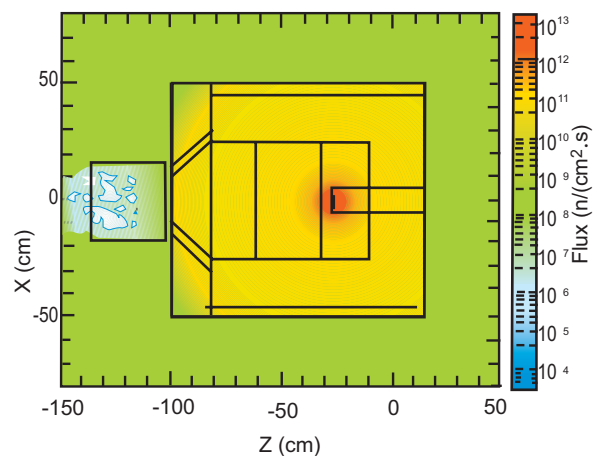


Fig. 4. Distribution of epithermal neutron flux in DBSA and water phantom

flux decreases from 1.0×10^9 n/(cm².s) to 1.0×10^7 n/cm².s. As for the neutron flux outside the phantom, it decreases 1.0×10^9 n/(cm².s) to 1.0×10^5 n/(cm².s).

Figure 5 shows the distribution of gamma particles in DBSA and phantom. The gamma flux around the beryllium target is 10^{12} gamma/(cm².s). The gamma particles are dominantly produced from interactions of protons with beryllium target through ${}^9_4\text{Be}(p, \alpha){}^6_3\text{Li}^*$ reactions. The ${}^6_3\text{Li}^*$ decays into ${}^6_3\text{Li}^*$ releasing γ (gamma). A small fraction of gamma ${}^9_4\text{Be}$ rays is also generated by capture reactions through ${}^9_4\text{Be}(n, n'\gamma){}^{10}_5\text{Be}$ reactions ${}^9_4\text{Be}$ and inelastic collision mechanisms in the form of ${}^9_4\text{Be}(n, n'\gamma){}^{10}_5\text{Be}$ reaction (Hu *et al.*, 2016). Gamma rays are also produced from the reaction of neutrons with aluminum through ${}^{27}_{13}\text{Al}(n, \gamma){}^{28}_{13}\text{Al}$ reactions. (Ivakhin *et al.*, 2011). Gamma rays enter the phantom and interact with H and O, losing their energy through mechanisms of photoelectric effect, Compton scattering, and pair production (Lamarsh and Baratta, 2001). These interactions cause gamma-ray flux to continually decline in the phantom. However, the gamma flux coming out from the DBSA is still quite high and hence a shielding is need to reduce the radiation. The increase gamma in the end of collimator could be caused by gamma radiation from the interaction of Cd and neutron.

Thermal neutron flux in water phantom. Figure 6 shows thermal neutron flux in the water phantom. The neutron thermal flux is distributed homogeneously throughout the volume of phantom. From the calculation using the MCNPX code the statistical uncertainty is found to be less than 5%. Such a value indicates the accuracy in calculations. A calculation by the MCNPX

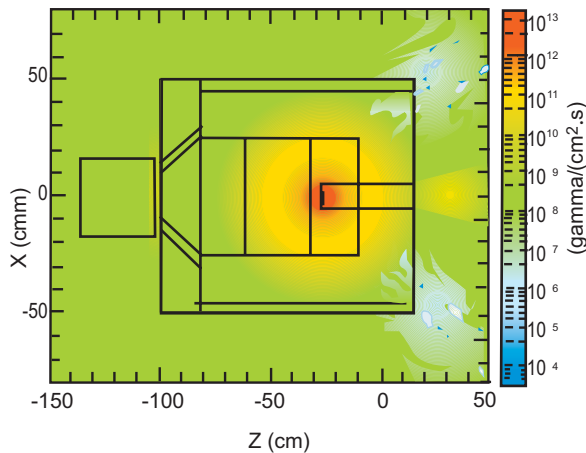


Fig. 5. Distribution of gamma in DBSA and water phantom.

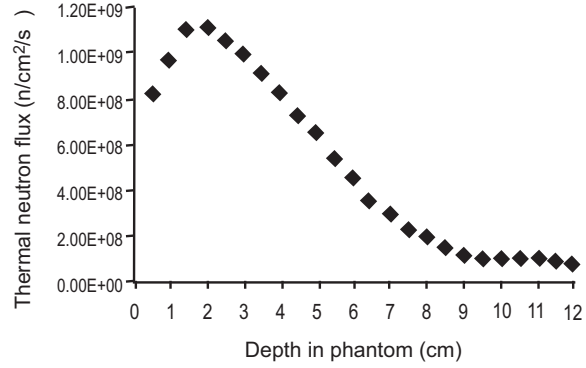


Fig. 6. Thermal neutron flux in the water phantom. The phantom is irradiated with epithermal neutrons from DBSA source.

is considered accurate when the statistical uncertainty is less than 10% (Pelowitz, 2005).

The maximum value of thermal neutron flux is 1.1×10^9 n/(cm².s), obtained at 2 cm deep from the surface of the phantom. Other researches also obtained a similar result (Morcos and Naguib, 2012; Tanaka *et al.*, 2011). The further deep epithermal neutron penetrate the phantom, the more increase in thermalization, causing the value of neutron flux to diminish. The value of thermal neutron flux at a depth of 5 and 12 cm, reaches 60% and 20% of its maximum value, respectively. The decrease in neutron flux is caused by the thermalization of neutrons with H (Shaaban and Albarhoum, 2015). Based on the result, the thermal neutrons has an effective range in phantom at 8 cm depth.

Based on the characteristic of neutron flux produced by the DBSA source and the behavior of neutrons in the phantom, the neutron beams produced by the DBSA can be considered as the main neutron source for BNCT. The intensity of epithermal neutron flux is 1.0×10^9 n/(cm².s), which can be used as the source of a 1-hour cancer therapy for maximum dose of 50 Gy (Capoulat *et al.*, 2014). The ability of thermal neutrons in a phantom shows that the neutron beams from the DBSA can be utilized as a neutron source for therapies of cancer situated at 2-8 cm. Some of the types of cancers that can be treated using the neutron source are head and neck cancer, glioblastoma, lung cancer, breast cancer, pancreas, brain tumor and sarcoma (Moss, 2014).

Conclusion

A Double-layer Beam Shaping Assembly (DBSA) is designed to produce epithermal neutrons for BNCT

purposes. The spectrum of neutron beams calculated at the location of the aperture has the following characteristics: the epithermal neutron flux of 1.0×10^9 n/(cm².s), the ratio of epithermal to the thermal and fast neutron flux of 344 and 85, respectively and the ratio of gamma-neutron dose to the epithermal neutron flux of 1.82×10^{-13} Gy.cm². This simulation study showed that epithermal neutron flux can penetrate up to 12 cm depth with the maximum flux of 1.1×10^9 n/(cm².s) at 2 cm depth. The flux of neutron at 5 cm depth is found to be 60%. The characteristics of neutron beams produced by the DBSA shows that they are adequate as the neutron source for BNCT, particularly for therapies of deeply-located cancers. However, the DBSA still produces gamma fluxes, in which a proper shielding to reduce the gamma flux is needed for safety in BNCT therapies.

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Conflict of Interest. The authors declare no conflict of interest

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