# Effect of Hydrochloric Acid on Different Ratios of Cement-sand Mortar 

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#### Abstract

Quality evaluation and quality assurance are the most important parameters which ensure the quality of any building material. For this reason, building materials are always analyzed by using different international test methods for checking and confirming their quality provided in the standard specifications. For this, first raw materials are examined (physically and chemically) and their results are compared with the international standard specifications to confirm their suitability. Cement-sand mortar cubes of different proportions are prepared and cured for 28 d . The physical suitability of mortar is ensured by calculating compressive strengths, while cement sand proportions are re-confirmed by adopting the test method BS 4550: 1970. The samples of known proportion were treated with the different concentrations of hydrochloric acid $(\mathrm{HCl})$ which vary from 5 M to 11 M and each molar solution was further classified as 1:7 and 1:9 and $1: 11$ dilution with water. Dilution of the HCl solution has proved to be ineffective in the proper decomposition of hydrates of cement. Cement contents do not dissolve in the solution completely and deviation in results is observed. The reactivity order of HCl solution with respect to its ratios is 1:7>1:9 $>1: 11$ for all molarities. Great variations in the results from $5 \mathrm{M}(1: 11)$ to $11 \mathrm{M}(1: 7)$ have been observed when graphs are plotted between mix ratio results and molarities. Linearity in a graph is achieved with a high concentration of HCl i-e $11 \mathrm{M}(1: 9)$, the solution gives the most accurate result. Accuracy in the results of mortar samples cannot be achieved utilizing different diluted HCl solutions. It is concluded from the data that by diluting HCl solution, test results drastically changed from standard values.


Keywords: mortar, British standards, hydrates of cement, cement-sand mix ratio, building material

## Introduction

A vast range of building materials is available due to the great diversity of their properties and requirements. Building materials are sub divided into separate groups due to their specific properties but their applications are pre-determined by their principal properties. Rational choice of material depends upon the comprehensive knowledge of the properties of materials for specific service conditions. A mixture of fine aggregate (sand) and binding materials (lime, gypsum, clay or cement) which turns to a paste by adding water which further turns to a hard mass when it sets is known as Mortar. It is mainly used in masonry construction to fill the gaps between the bricks and blocks as a binding material. In addition, it is also used as rendering to produce a better aesthetic look (Joseph, 1850). Mortar is usually defined by its composition rather than properties and proportions of ingredients are generally taken in weight

[^0]or volume. There are different types of mortars commonly used such as cement mortar, lime mortar, lime cement mortar, etc. Cement-sand mortar is also called cement mortar which has been used in more than ten thousand buildings (houses, hospitals, schools, etc.) only in Pakistan.

Cement is used as a binder in mortar. It is mostly used in bricks or blocks based structures for joining building units (Raziuddin, 1967). In 1824, Joseph Aspedin of Yorkshire (United Kingdom) patented a new modern method of that time to manufacture cement by the heating mixture of limestone and clay at high temperature in a furnace.

Cement-sand and water are mixed to prepare cement mortars of specific proportions required for a specific project. Portland cement mortars were found productive in stiffness, bond strength, water retention, flexibility than all other types (Pavia and Brennan, 2019). It has been observed that there are some factors such as the number of water vapours and porosity effects on the
properties of cement (Zhang et al., 2018). It has been studied that cementitious gel had a strong affinity towards the water and it contributes to strength (Powers, 1958) .

The strength of cement mortars depends upon cement sand proportion and the strength of joining materials like blocks, bricks etc. Cement mortars should be strong enough to resist abrasion, erosion and other factors affecting durability. If the strength of mortars is higher than the strength of block units or bricks, settlement or shrinkage cracks may become large (Varghese, 2005). The compressive strength of different class mortars was also monitored (Eskandari-Naddaf and Kazemi, 2017). Different methods have been used to test the basic physico-chemical properties, reactivity and performance of cement (Zaleska et al., 2018). Different proportions of cement and sand are fixed for different requirements such as 1:3 mortar ratio is used in an arch and pointing work. Whereas, a higher ratio of mortar like $1: 6$ is suitable for brickwork. The selection of the mortar ratio is mainly dependent on compressive strength (Singh et al., 2015).

The compressive strength of Portland cement can be increased by using the blend of $30 \%$ natural Pozzolana and $20 \%$ of limestone filler with Portland cement (Forde 2009; Kakali et al., 2000). This blend was found flexural, compressive and resistant against acid and sulfate attack (Ghrici et al., 2007). The quality of cement mortar is tested either checking its compressive strength or mix ratio analysis done by different techniques such as thermal, gravimetric or X-ray diffraction analysis (Genestar et al., 2006).

In the present study the analysis is carried out by gravimetric method (Test Method BS 4550: 1970). This method is used till date in all Pakistani government testing laboratories even in India and Bangladesh. In this method HCl is used as a separating medium that separates binder and aggregate from mortar (Alvarez
et al., 1999). It has been observed that different mortars react differently with varying the concentrations of HCl (De Ceukelaire, 1992). Test Method BS 4550: 1970 (Smith and Halliwell, 1979) does not tell clearly about the exact concentration of HCl to be used for the analysis of mortar. Here detailed and comprehensive study is conducted to signify the importance of solvent effect ( HCl dilution) on standard mortar samples and explained that how by changing the slight concentration of HCl the test results drastically deviate (Vayghan et al., 2013; Quarcioni and Cincotto, 2006).

## Materials and Methods

Water. Water used in this research was chemically tested before its use as per ASTM methods and BS 1377 part 3 to confirm its suitability for the preparation of cement mortars and its analysis is given in Table 1.

Cement. Ordinary Portland Cement (OPC) with the trademark "Maple Leaf Cement" was purchased from the local market of township Lahore Pakistan. To ensure the quality of cement both physical testing following ASTM C109, ASTM C191, ASTM C430, ASTM C151 /C151M, using specification ASTM C183 and chemical testing in accordance British Standard BS 4550-2:1970 were conducted Table 2.

Fine aggregate (sand). Sand from different sources (Ravi Sand, Chenab Sand and Ghandapur, Kasur Sand)

Table 1. Chemical analysis of water

| Description of tests | Determined <br> values | Permissible <br> limits for <br> construction <br> purposes |
| :--- | :--- | :--- |
| Total soluble salts | $0.01 \%$ | $0.15 \%$ |
| Total sulphate content | Traces | $0.05 \%$ |
| Total chlorides content | Nil | $0.036 \%$ |
| pH-value | 7.2 | 6 to 8 |
| Total solid content | Nil | $0.05 \%$ |

Table 2. Description of cement-testing

| Description of tests | Test method | Determined values | Permissible limits |
| :--- | :--- | :--- | :--- |
| Compressive strength (3 d) | ASTM C109-16a | 2295 Psi | 1740 Psi |
| Compressive strength (7 d) |  | 2962 Psi | 2760 Psi |
| Initial setting time $(\mathrm{min})$ | ASTM C191-19 | 209 min | Not less than 45 min |
| Final setting time $(\mathrm{min})$ |  | 351 min | Not more than 375 min |
| Fineness | ASTM C430-08 | $98.8 \%$ | Not less than $90 \%$ |
| Cement expansion | ASTM C151 / C151M-09 | 0.833 mm | $10 \mathrm{~mm}(\max )$ |

was collected from respective areas and tested in Laboratory. After respective testing of all these samples, they were found unfit to use for the preparation of cement mortars according to ASTM C144-04 (Standard Specification for Aggregate for Masonry Mortar, 2006).
This problem was solved by using manufactured sand which fulfilled all the limits given in ASTM C144-04 (Standard Specification for Aggregate for Masonry Mortar) reported by Ayan et al. (2015). The most volume of mortar is based on fine aggregate (sand). It was observed that the grading of sand caused an impact on the properties of masonry units reported by (Ahmad, 2013; Reddy and Gupta, 2008).

Preparation of cement mortar sample. Three cement mortar samples of 1:4, 1:5 and 1:6 proportions (cement: sand) were prepared using a specific quantity of water ( 0.484 water: cement) in mixer machine and nine cubes of ( 2 " $\times 2$ " $\times 2$ ") dimensions of each proportion were separately filled and kept at room temperature for one day. The cubes were cured in the water bath for 28 d . After determination of compressive strengths of cubes, crushed samples were kept in an oven at $100^{\circ} \mathrm{C}$ for 24 $h$ for drying. Samples were then cooled at room temperature and converted into a powder that can pass through sieve no. 40. This powder sample of each proportion was analyzed chemically for mix ratio determination and solvent effect.

Testing methodology. Removal of unreacted sand as insoluble residue. The cement and sand are easily separated from cement mortar by using HCl . All components of cement and trace of sand form their respective chlorides which are soluble in water, while major components of sand remain unreacted with HCl . Three cement mortar samples of $1: 4,1: 5$ and $1: 6$ proportions ( 50 g of each) were treated with the different HCl solutions of different molarities ranging from 5 M-11 M and different ratios such as 1:7, 1:9 and 1:11 $(\mathrm{HCl}$ : water). When HCl comes in contact with the mortar, it penetrates the hydrates of cement (gel type and crystal) where it reacts. Chlorides of metals get dissolved but crystalline silica, unreacted hydrates and some complexes remain insoluble. Samples were then filtered. The residue was washed three times to make sure that no cement contents remain in the residue. The unreacted materials obtained from all three mortar samples were properly washed with HCl solution of similar molarities and ratio and collected over filter paper as insoluble residue. It was properly dried in an oven and weighed again.

Removal of soluble silica. The filtrate obtained from the above step containing reactive silica. It has to be removed for the accurate measurement of lime in the sample. So, the drying method was used which converts the reactive silica into nonreactive silica which is easily removed in the form of a gel. The volume of the filtrate was made up to 1000 mL using distilled water. Out of which 50 mL was taken and heated on water bath till complete dry. The sample was then kept in an oven at $100^{\circ} \mathrm{C}$ for 1 h . Then 5 mL of respective molar HCl and 40 mL of distilled water were added to the sample and gently heated. It was then filtered and the residue was washed with hot water three times.

Removal of metals in the form of hydroxides except for calcium. Different metals are present in the above filtrate in the form of chlorides $\left(\mathrm{NaCl}, \mathrm{FeCl}_{2}, \mathrm{FeCl}_{3}\right.$, $\left.\mathrm{AlCl}_{3}, \mathrm{MgCl}_{2}, \mathrm{CaCl}_{2}, \mathrm{KCl}\right)$. All metallic chlorides are converted into metallic hydroxides except $\mathrm{CaCl}_{2}$ by treating the filtrate with $\mathrm{NH}_{4} \mathrm{O}$ and $\mathrm{NH}_{4} \mathrm{OH}$. It was then filtered and the residue was washed thrice.
Conversion of calcium in the form of calcium oxalate. The filtrate from the above step was heated with 50 mL ( $5 \% \mathrm{~m} / \mathrm{v}$ ) ammonium oxalate and 5 mL ammonia solution (1:2) till boiling. Precipitates were allowed to settles for 30 min and then filtered. Ammonium oxalate in the presence of ammonium hydroxide converted the soluble calcium into insoluble calcium oxalate.

Ignition of calcium oxalate. Calcium oxalate obtained in the above step ignited in the electric furnace at 1000 ${ }^{\circ} \mathrm{C}$, where calcium oxalate is converted into calcium oxide.

## Result and Discussion

The reactivity of HCl solutions drastically changes from $11 \mathrm{M}(1: 7)$ to $5 \mathrm{M}(1: 11)$. Linearity in the curves of $1: 7$ and $1: 9$ has been observed till 7 M . It gives the best understanding of the solvent effect. After 7 M graph becomes straight because of the low gradient potential and less penetrating ability of HCl to react with hydrates of cement. 1:11 curve provides the best knowledge about the limiting reactivity and solvent effect of HCl in comparison with 1:7 curves, which is shown in Table 3 and Fig. 1.
In the light of evaluated data of 1:4 cement mortar samples, it is observed that both the test results of insoluble residue and lime show a similar increasing reactivity trend of Hydrochloric acid from $5 \mathrm{M}(1: 11)$ solution to $11 \mathrm{M}(1: 7)$ and provide the best information to understand the solvent effect of different solutions

Table 3. Determination of cement sand proportion based on insoluble residue (standard cement-sand proportion used 1: 4)

| HCl <br> molarities | HCl <br> Dilution | Weight of filter paper (g) | Sum of the weight of filter paper (g) | Weight of filter paper and residue (g) | Weight of filter paper papers and residue (g) | Sum of the weight of filter papers and residue | Weight of residue (g) | $\begin{aligned} & \text { Sand } \\ & \% \end{aligned}$ | Cement \% | Mix ratio result (By weight) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  | Cement | Sand |
| 11 M | 1:7 | 1.4280 | 4.2844 | 12.5838 | 12.5838 | 40.9154 | 36.6310 | 73.2620 | 26.7380 | 1.00 | 2.74 |
|  |  | 1.4356 |  | 15.6014 | 15.6014 |  |  |  |  |  |  |
|  |  | 1.4208 |  | 12.7302 | 12.7302 |  |  |  |  |  |  |
|  | 1:9 | 1.3821 | 4.1992 | 11.8642 | 11.8642 | 41.6047 | 37.4055 | 74.8110 | 25.1890 | 1.00 | 2.97 |
|  |  | 1.3955 |  | 14.9768 | 14.9768 |  |  |  |  |  |  |
|  |  | 1.4216 |  | 14.7637 | 14.7637 |  |  |  |  |  |  |
|  | 1:11 | 1.3991 | 4.2193 | 11.8642 | 11.8642 | 42.3990 | 38.1797 | 76.3594 | 23.6406 | 1.00 | 3.23 |
|  |  | 1.3864 |  | 14.9768 | 14.9768 |  |  |  |  |  |  |
|  |  | 1.4338 |  | 15.5580 | 15.5580 |  |  |  |  |  |  |
| 10 M | 1:7 | 1.4212 | 4.2314 | 9.9657 | 9.9657 | 41.7626 | 37.5312 | 75.0624 | 24.9376 | 1.00 | 3.01 |
|  |  | 1.3856 |  | 13.3563 | 13.3563 |  |  |  |  |  |  |
|  |  | 1.4246 |  | 18.4406 | 18.4406 |  |  |  |  |  |  |
|  | $1: 9$ | 1.4199 | 4.2740 | 14.3279 | 14.3279 |  |  |  |  |  |  |
|  |  | 1.4081 |  | 11.1321 | 11.1321 | 42.1675 | 37.8935 | 75.7870 | 24.2130 | 1.00 | 3.13 |
|  |  | 1.4460 |  | 16.7075 | 16.7075 |  |  |  |  |  |  |
|  |  | 1.4453 |  | 18.0442 | 18.0442 |  |  |  |  |  |  |
|  | 1:11 | 1.4654 | 4.3404 | 13.4131 | 13.4131 | 42.8725 | 38.5321 | 77.0642 | 22.9358 | 1.00 | 3.36 |
|  |  | 1.4297 |  | 11.4152 | 11.4152 |  |  |  |  |  |  |
| 9 M |  | 1.4542 | 4.3681 | 17.2583 | 17.2583 | 42.9786 | 38.6105 | 77.2210 | 22.7790 | 1.00 | 3.39 |
|  | 1:7 | 1.4480 |  | 12.3448 | 12.3448 |  |  |  |  |  |  |
|  | $1: 9$ | 1.4659 |  | 13.3755 | 13.3755 |  |  |  |  |  |  |
|  |  | 1.4602 | 4.3238 | 17.1196 | 17.1196 | 43.2373 | 38.9135 | 77.8270 | 22.1730 | 1.00 | 3.51 |
|  |  | 1.4202 |  | 13.5973 | 13.5973 |  |  |  |  |  |  |
|  |  | 1.4434 |  | 12.5204 | 12.5204 |  |  |  |  |  |  |
|  |  | 1.4546 |  | 12.8866 | 12.8866 |  |  |  |  |  |  |
|  | 1:11 | 1.4388 | 4.3138 | 16.4941 | 16.4941 | 43.5147 | 39.2009 | 78.4018 | 21.5982 | 1.00 | 3.63 |
|  |  | 1.4204 |  | 14.1340 | 14.1340 |  |  |  |  |  |  |
| 8 M | 1:7 | 1.4137 | 4.2107 | 14.6805 | 14.6805 | 43.0250 | 38.8143 | 77.6286 | 22.3714 | 1.00 | 3.47 |
|  |  | 1.3940 |  | 14.4277 | 14.4277 |  |  |  |  |  |  |
|  |  | 1.4030 |  | 13.9168 | $13.9168$ |  |  |  |  |  |  |
|  |  | 1.4042 | 4.2184 | 13.7804 | 13.7804 |  |  |  |  |  |  |
|  | $1: 9$ | 1.3932 |  | 17.6257 | 17.6257 | 43.6476 | 39.4292 | 78.8584 | 21.1416 | 1.00 | 3.73 |
|  |  | 1.4210 |  | 12.2415 | 12.2415 |  |  |  |  |  |  |
|  |  | 1.3995 |  | 11.8452 | 11.8452 |  |  |  |  |  |  |
|  | 1:11 | 1.4620 | 4.3291 | 14.0043 | 14.0043 | 44.4672 | 40.1381 | 80.2762 | 19.7238 | 1.00 | 4.07 |
|  |  | 1.4676 |  | 18.6177 | 18.6177 |  |  |  |  |  |  |
| 7 M | 1:7 | 1.4382 | 4.3018 | 12.4708 | 12.4708 | 43.4793 | 39.1775 | 78.3550 | 21.6450 | 1.00 | 3.62 |
|  |  | 1.4225 |  | 17.7391 | 17.7391 |  |  |  |  |  |  |
|  |  | 1.4411 |  | 13.2694 | 13.2694 |  |  |  |  |  |  |
|  |  | 1.3794 |  | 18.8499 | 18.8499 |  |  |  |  |  |  |
|  | 1:9 | 1.4107 | 4.1928 | 12.4962 | 12.4962 | 43.7927 | 39.5999 | 79.1998 | 20.8002 | 1.00 | 3.81 |
|  |  | 1.4027 |  | 12.4466 | 12.4466 |  |  |  |  |  |  |
|  |  | 1.4154 |  | 16.0575 | 16.0575 |  |  |  |  |  |  |
|  | 1:11 | 1.4469 | 4.3008 | $15.9798$ | $15.9798$ | 44.7406 | 40.4398 | 80.8796 | 19.1204 | 1.00 | 4.23 |
|  |  | 1.4385 |  | 12.7033 | $12.7033$ |  |  |  |  |  |  |
|  |  | 1.4526 |  | 16.7521 | 16.7521 |  |  |  |  |  |  |
|  | 1:7 | 1.4427 | 4.3202 | 12.4127 | 12.4127 | 43.6364 | 39.3162 | 78.6324 | 21.3676 | 1.00 | 3.68 |
|  |  | 1.4249 |  | 14.4716 | 14.4716 |  |  |  |  |  |  |
|  |  | 1.4433 |  | 14.1765 | 14.1765 |  |  |  |  |  |  |
| 6 M | 1:9 | 1.4084 | 4.2742 | 15.4967 | 15.4967 | 43.9428 | 39.6686 | 79.3372 | 20.6628 | 1.00 | 3.84 |
|  |  | 1.4225 |  | 14.2696 | 14.2696 |  |  |  |  |  |  |
|  |  | 1.4662 |  | 16.7655 | 16.7655 |  |  |  |  |  |  |
|  | 1:11 | 1.4395 | 4.3774 | 12.6468 | 12.6468 | 45.2570 | 40.8796 | 81.7592 | 18.2408 | 1.00 | 4.48 |
|  |  | 1.4717 |  | 15.8447 | 15.8447 |  |  |  |  |  |  |


of hydrochloric acid with the same sample. The reactivity order with respect to their ratios is $1: 7>1: 9>1: 11$. Moreover, the determination of the mix ratio of cement and sand in the cement mortar sample is based on the lime (calcium oxide) content present in the respective sample. For a cement mortar sample, the determined lime (calcium oxide) content may deviate from true value up to $4 \%$ for the cement.

Furthermore, this tolerance provides a range for mix ratio (1:4) cement mortar samples i.e. from1:3.81 to 1 : 4.22. By comparing the test results of the Table 4 and Fig. 2 with the above mentioned range, it was noticed that the test results of $11 \mathrm{M}(1: 9)$ and $10 \mathrm{M}(1: 7)$ solutions are within the calculated range and the remaining test
results indicate small variation in the HCl solution drastically changes the test results, while $11 \mathrm{M}(1: 9)$ solution gives the most accurate results.

The reactivity pattern is the same as discussed in the results of 1:4 cement mortar samples but the range for 1:5 cement mortar samples is calculated from 1:4.77 to $1: 5.25$. By comparing the test results of the above mentioned range, it was investigated that again the test results of $11 \mathrm{M}(1: 9)$ and $10 \mathrm{M}(1: 7)$ solutions are within the calculated range and remaining test results indicates small variation in the HCl solution drastically changes the test results while $11 \mathrm{M}(1: 9)$ solution gives the most accurate results, which is shown in Table 5-6 and Fig. 3-4.

Table 4. Effect of dillution of HCL on mix ratio (1:4 cement mortar lime based)

| HCl <br> molarity | HCl <br> dilution | Identification <br> mark of <br> platinum <br> crucible | Weight of <br> platinum <br> crucible <br> $(\mathrm{g})$ | Weight of <br> platinum <br> crucible and | Weight of <br> residue <br> $(\mathrm{g})$ | \%age of Lime <br> $(\mathrm{g})$ |  | \%age of <br> sand | Mix ratio result <br> (By weight) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |  |  |  |  |

Table 5. Effect of dilution of HCl on max ratio 1:5 cement mortar insoluble residue

| Sr. no. | HCl molarity | HCl <br> dilution | Weight of filter paper (g) | Sum of the weight of filter papers <br> (g) | Weight of filter paper and residue (g) | Sum of the weight of filter papers and residue (g) | Weight of residue <br> (g) | $\begin{aligned} & \text { Sand } \\ & \% \end{aligned}$ | Cement \% | Mix ratio <br> (By wei $\qquad$ <br> Cement | result <br> t) <br> Sand |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B001 | 11 M | 1:7 | 1.3922 | 4.2255 | 11.9473 | 42.3439 | 38.1184 | 76.2368 | 23.7632 | 1.00 | 3.21 |
| B002 |  |  | 1.4186 |  | 12.5835 |  |  |  |  |  |  |
| B003 |  |  | 1.4147 |  | 17.8131 |  |  |  |  |  |  |
| B004 |  | 1:9 | 1.4338 | 4.3197 | 15.1090 | 43.0338 | 38.7141 | 77.4282 | 22.5718 | 1.00 | 3.43 |
| B005 |  |  | 1.4474 |  | 10.7333 |  |  |  |  |  |  |
| B006 |  |  | 1.4385 |  | 17.1915 |  |  |  |  |  |  |
| B007 |  |  | 1.4397 |  | 13.7237 |  |  |  |  |  |  |
| B008 |  | 1:11 | 1.4275 | 4.2922 | 16.9944 | 43.7410 | 39.4488 | 78.8976 | 21.1024 | 1.00 | 3.74 |
| B009 |  |  | 1.4250 |  | 13.0229 |  |  |  |  |  |  |
| B010 |  |  | 1.4257 |  | 17.2223 |  |  |  |  |  |  |
| B011 |  | 1:7 | 1.4181 | 4.2762 | 13.5656 | 42.8836 | 38.6074 | 77.2148 | 22.7852 | 1.00 | 3.39 |
| B012 |  |  | 1.4324 |  | 12.0957 |  |  |  |  |  |  |
| B013 |  |  | 1.4147 |  | 13.8115 |  |  |  |  |  |  |
| B014 | 10 M | 1:9 | 1.4287 | 4.2720 | 14.4833 | 43.2154 | 38.9434 | 77.8868 | 22.1132 | 1.00 | 3.52 |
| B015 |  |  | 1.4286 |  | 14.9206 |  |  |  |  |  |  |
| B016 |  |  | 1.4399 |  | 18.1116 |  |  |  |  |  |  |
| B017 |  | 1:11 | 1.4501 | 4.3083 | 12.8893 | 44.3067 | 39.9984 | 79.9968 | 20.0032 | 1.00 | 4.00 |
| B018 |  |  | 1.4183 |  | 13.3058 |  |  |  |  |  |  |
| B019 |  |  | 1.4665 |  | 17.3543 |  |  |  |  |  |  |
| B020 |  | 1:7 | 1.4332 | 4.3538 | 10.9999 | 43.8545 | 39.5007 | 79.0014 | 20.9986 | 1.00 | 3.76 |
| B021 |  |  | 1.4541 |  | 15.5003 |  |  |  |  |  |  |
| B022 |  |  | 1.4349 |  | 12.1885 |  |  |  |  |  |  |
| B023 | 9 M | 1:9 | 1.4295 | 4.2783 | 15.1424 | 44.1447 | 39.8664 | 79.7328 | 20.2672 | 1.00 | 3.93 |
| B024 |  |  | 1.4139 |  | 16.8138 |  |  |  |  |  |  |
| B025 |  |  | 1.4353 |  | 18.2916 |  |  |  |  |  |  |
| B026 |  | 1:11 | 1.4391 | 4.3141 | 13.1025 | 45.7118 | 41.3977 | 82.7954 | 17.2046 | 1.00 | 4.81 |
| B027 |  |  | 1.4397 |  | 14.3177 |  |  |  |  |  |  |
| B028 |  |  | 1.4277 |  | 11.3080 |  |  |  |  |  |  |
| B029 |  | 1:7 | 1.4389 | 4.3111 | 15.4827 | 44.2078 | 39.8967 | 79.7934 | 20.2066 | 1.00 | 3.95 |
| B030 |  |  | 1.4445 |  | 17.4171 |  |  |  |  |  |  |
| B031 |  |  | 1.4442 |  | 16.4886 |  |  |  |  |  |  |
| B032 | 8 M | 1:9 | 1.4514 | 4.3383 | 14.4650 | 45.3684 | 41.0301 | 82.0602 | 17.9398 | 1.00 | 4.57 |
| B033 |  |  | 1.4427 |  | 14.4148 |  |  |  |  |  |  |
| B034 |  |  | 1.4275 |  | 12.4021 |  |  |  |  |  |  |
| B035 |  | 1:11 | 1.4364 | 4.3231 | 17.3865 | 46.6465 | 42.3234 | 84.6468 | 15.3532 | 1.00 | 5.51 |
| B036 |  |  | 1.4592 |  | 16.8579 |  |  |  |  |  |  |
| B037 |  |  | 1.4441 |  | 15.3571 |  |  |  |  |  |  |
| B038 |  | 1:7 | 1.4562 | 4.3463 | 12.8373 | 44.6359 | 40.2896 | 80.5792 | 19.4208 | 1.00 | 4.15 |
| B039 | 7 M |  | 1.4460 |  | 16.4415 |  |  |  |  |  |  |
| B040 |  | 1:9 | 1.4453 | 4.3404 | 12.2328 | 45.5595 | 41.2191 | 82.4382 | 17.5618 | 1.00 | 4.69 |
| B041 |  |  | 1.4654 |  | 17.1628 |  |  |  |  |  |  |
| B042 |  |  | 1.4297 |  | 16.1639 |  |  |  |  |  |  |
| B043 |  | 1:11 | 1.4369 | 4.3104 | 18.1839 | 46.7782 | 42.4678 | 84.9356 | 15.0644 | 1.00 | 5.64 |
| B044 |  |  | 1.4351 |  | 15.2159 |  |  |  |  |  |  |
| B045 |  |  | 1.4384 |  | 13.3784 |  |  |  |  |  |  |
| B046 | 6 M | 1:7 | 1.4242 | 4.2687 | 14.3085 | 44.8167 | 40.5480 | 81.0960 | 18.9040 | 1.00 | 4.29 |
| B047 |  |  | 1.4186 |  | 17.2444 |  |  |  |  |  |  |
| B048 |  |  | 1.4259 |  | 13.2638 |  |  |  |  |  |  |
| B049 |  | 1:9 | 1.4444 | 4.4567 | 11.9722 | 45.7357 | 41.2790 | 82.5580 | 17.4420 | 1.00 | 4.73 |
| B050 |  |  | 1.5521 |  | 15.5998 |  |  |  |  |  |  |


| B051 |  |  | 1.4602 |  | 18.1637 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B052 |  | 1:11 | 1.3802 | 4.1982 | 15.6427 | 46.6881 | 42.4899 | 84.9798 | 15.0202 | 1.00 | 5.66 |
| B053 |  |  | 1.4234 |  | 13.8789 |  |  |  |  |  |  |
| B054 |  |  | 1.3946 |  | 17.1665 |  |  |  |  |  |  |
| B055 | 5 M | 1:7 | 1.4158 | 4.2287 | 18.2605 | 44.8976 | 40.6689 | 81.3378 | 18.6622 | 1.00 | 4.36 |
| B056 |  |  | 1.4204 |  | 10.4268 |  |  |  |  |  |  |
| B057 |  |  | 1.3925 |  | 16.2103 |  |  |  |  |  |  |
| B058 |  | 1:9 | 1.4141 | 4.2431 | 16.9674 | 45.6863 | 41.4432 | 82.8864 | 17.1136 | 1.00 | 4.84 |
| B059 |  |  | 1.4282 |  | 12.2923 |  |  |  |  |  |  |
| B060 |  |  | 1.4008 |  | 16.4266 |  |  |  |  |  |  |
| B061 |  | 1:11 | 1.4023 | 4.2344 | 13.1877 | 46.8452 | 42.6108 | 85.2216 | 14.7784 | 1.00 | 5.77 |
| B062 |  |  | 1.4178 |  | 15.9169 |  |  |  |  |  |  |
| B063 |  |  | 1.4143 |  | 17.7406 |  |  |  |  |  |  |



Fig. 1. Effect of dilutions of HCl on mix ratio ( $1: 4$ cement mortar insoluble residues).


Fig. 2. Effect of dilutions of HCl on mix ratio (1:4 cement mortar lime based).


Fig. 3. Effect of dilutions of HCl on mix ratio (1:5 cement mortar insoluble residues).


Fig. 4. Effect of dilutions of HCl on mix ratio (1:5 cement mortar lime-based).

The reactivity pattern is the same as discussed in the results of 1:4 and 1:5 cement mortar samples but the range for $1: 6$ cement mortar samples is calculated from $1: 5.73$ to $1: 6.29$. By comparing the test results of the above mentioned range, it was observed that again the
test results of $11 \mathrm{M}(1: 9)$ and $10 \mathrm{M}(1: 7)$ solutions are within the calculated range and the remaining test results, indicate small variation in the HCl solution drastically changes the test results while $11 \mathrm{M}(1: 9)$ solution gives the most accurate results (Table 7\&8 and Fig. 5\&6).

Table 6. Determination of cement-sand proportion based on lime (standard cement-sand proportion used 1:5)

| HCl molarity | HCl <br> dilution | Identification <br> mark of <br> platinum <br> crucible | Weight of platinum crucible <br> (g) | Weight of platinum crucible and residue (g) | Weight of residue <br> (g) | \%age of Lime |  | \%age of sand | Mix ratio result (by weight) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | Cement | Sand |
| 11 M | 1:7 | 1 | 42.9728 | 43.2591 | 0.2863 | 11.4520 | 17.5644 | 82.4356 | 1.00 | 4.69 |
|  | 1:9 | 2 | 43.8753 | 44.1465 | 0.2712 | 10.8480 | 16.6380 | 83.3620 | 1.00 | 5.01 |
|  | 1:11 | 3 | 41.5671 | 41.8184 | 0.2513 | 10.0520 | 15.4172 | 84.5828 | 1.00 | 5.49 |
| 10 M | 1:7 | 4 | 44.6622 | 44.9255 | 0.2633 | 10.5320 | 16.1534 | 83.8466 | 1.00 | 5.19 |
|  | 1:9 | 5 | 40.4584 | 40.7094 | 0.251 | 10.0400 | 15.3988 | 84.6012 | 1.00 | 5.49 |
|  | 1:11 | 6 | 37.7162 | 37.9473 | 0.2311 | 9.2440 | 14.1779 | 85.8221 | 1.00 | 6.05 |
| 9 M | 1:7 | 7 | 43.4481 | 43.6975 | 0.2494 | 9.9760 | 15.3006 | 84.6994 | 1.00 | 5.54 |
|  | 1:9 | 8 | 44.9822 | 45.2220 | 0.2398 | 9.5920 | 14.7117 | 85.2883 | 1.00 | 5.80 |
|  | 1:11 | 9 | 23.6818 | 23.8958 | 0.214 | 8.5600 | 13.1288 | 86.8712 | 1.00 | 6.62 |
| 8 M | 1:7 | 10 | 41.7884 | 42.0242 | 0.2358 | 9.4320 | 14.4663 | 85.5337 | 1.00 | 5.91 |
|  | 1:9 | 11 | 26.5280 | 26.7496 | 0.2216 | 8.8640 | 13.5951 | 86.4049 | 1.00 | 6.36 |
|  | 1:11 | 12 | 68.9158 | 69.1215 | 0.2057 | 8.2280 | 12.6196 | 87.3804 | 1.00 | 6.92 |
| 7 M | 1:7 | 1 | 42.9727 | 43.1892 | 0.2165 | 8.6600 | 13.2822 | 86.7178 | 1.00 | 6.53 |
|  | 1:9 | 2 | 43.8751 | 44.0824 | 0.2073 | 8.2920 | 12.7178 | 87.2822 | 1.00 | 6.86 |
|  | 1:11 | 3 | 41.5669 | 41.7523 | 0.1854 | 7.4160 | 11.3742 | 88.6258 | 1.00 | 7.79 |
| 6 M | 1:7 | 4 | 44.6619 | 44.8768 | 0.2149 | 8.5960 | 13.1840 | 86.8160 | 1.00 | 6.58 |
|  | 1:9 | 5 | 40.4582 | 40.6638 | 0.2056 | 8.2240 | 12.6135 | 87.3865 | 1.00 | 6.93 |
|  | 1:11 | 6 | 37.7161 | 37.8997 | 0.1836 | 7.3440 | 11.2638 | 88.7362 | 1.00 | 7.88 |
| 5 M | 1:7 | 7 | 43.4477 | 43.6623 | 0.2146 | 8.5840 | 13.1656 | 86.8344 | 1.00 | 6.60 |
|  | 1:9 | 8 | 44.9814 | 45.1863 | 0.2049 | 8.1960 | 12.5706 | 87.4294 | 1.00 | 6.96 |
|  | 1:11 | 9 | 23.6816 | 23.8644 | 0.1828 | 7.3120 | 11.2147 | 88.7853 | 1.00 | 7.92 |



Fig. 5. Effect of dilutions of HCl on mix ratio (1:6 cement mortar insoluble residues).


Fig. 6. Effect of dilutions of HCl on mix ratio (1:6 cement mortar lime-based).

Table 7. Determination of cement-sand proportion based on insoluble residue (standard cement sand proportion used 1:6)

| HCl molarity | HCl <br> dilution | Weight of filter paper (g) | Sum of the weight of filter papers <br> (g) | Weight of filter paper and residue (g) | Sum of the weight of filter papers and residue (g) | Weight of residue (g) | $\begin{aligned} & \text { Sand } \\ & \% \end{aligned}$ | Cement $\%$ | Mix rati <br> (by weig <br> Cement | Sasult |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11 M | 1:7 | 1.3865 | 4.1492 | 14.9321 | 44.4801 | 40.3309 | 80.6618 | 19.3382 | 1.00 | 4.17 |
|  |  | 1.3982 |  | 12.8452 |  |  |  |  |  |  |
|  |  | 1.3645 |  | 16.7028 |  |  |  |  |  |  |
|  | $1: 9$ | 1.4034 | 4.2470 | 12.6896 | 44.9745 | 40.7275 | 81.4550 | 18.5450 | 1.00 | 4.39 |
|  |  | 1.4281 |  | 17.1857 |  |  |  |  |  |  |
|  |  | 1.4155 |  | 15.0992 |  |  |  |  |  |  |
|  | 1:11 | 1.3949 | 4.2350 | 18.2587 | 45.4209 | 41.1859 | 82.3718 | 17.6282 | 1.00 | 4.67 |
|  |  | 1.4256 |  | 13.9517 |  |  |  |  |  |  |
|  |  | 1.4145 |  | 13.2105 |  |  |  |  |  |  |
| 10 M | 1:7 | 1.3938 | 4.2311 | 16.3579 | 44.8319 | 40.6008 | 81.2016 | 18.7984 | 1.00 | 4.32 |
|  |  | 1.4284 |  | 15.8306 |  |  |  |  |  |  |
|  |  | 1.4089 |  | 12.6434 |  |  |  |  |  |  |
|  | $1: 9$ | 1.4112 | 4.2153 | 18.7756 | 45.1369 | 40.9216 | 81.8432 | 18.1568 | 1.00 | 4.51 |
|  |  | 1.4058 |  | 15.5369 |  |  |  |  |  |  |
|  |  | 1.3983 |  | 10.8244 |  |  |  |  |  |  |
|  | 1:11 | 1.3895 | 4.1812 | 11.8882 | 45.8037 | 41.6225 | 83.2450 | 16.7550 | 1.00 | 4.97 |
|  |  | 1.3984 |  | 17.7642 |  |  |  |  |  |  |
|  |  | 1.3933 |  | 16.1513 |  |  |  |  |  |  |
| 9 M | 1:7 | 1.3777 | 4.1565 | 17.0801 | 45.1966 | 41.0401 | 82.0802 | 17.9198 | 1.00 | 4.58 |
|  |  | 1.3842 |  | 14.9985 |  |  |  |  |  |  |
|  |  | 1.3946 |  | 13.1180 |  |  |  |  |  |  |
|  | $1: 9$ | 1.4135 | 4.2281 | 12.9901 | 45.6802 | 41.4521 | 82.9042 | 17.0958 | 1.00 | 4.85 |
|  |  | 1.3907 |  | 18.1333 |  |  |  |  |  |  |
|  |  | 1.4239 |  | 14.5568 |  |  |  |  |  |  |
|  | 1:11 | 1.4338 | 4.2558 | 16.9003 | 46.4336 | 42.1778 | 84.3556 | 15.6444 | 1.00 | 5.39 |
|  |  | 1.4154 |  | 12.2692 |  |  |  |  |  |  |
|  |  | 1.4066 |  | 17.2641 |  |  |  |  |  |  |
|  |  | 1.4153 |  | 11.8234 |  |  |  |  |  |  |
|  | 1:7 | 1.3944 | 4.2054 | 13.9847 | 45.5292 | 41.3238 | 82.6476 | 17.3524 | 1.00 | 4.76 |
|  |  | 1.3957 |  | 19.7211 |  |  |  |  |  |  |
|  |  | 1.4111 |  | 12.5412 |  |  |  |  |  |  |
| 8 M | $1: 9$ | 1.4355 | 4.2739 | 17.8194 | 45.9043 | 41.6304 | 83.2608 | 16.7392 | 1.00 | 4.97 |
|  |  | 1.4273 |  | 15.5437 |  |  |  |  |  |  |
|  |  | 1.4172 |  | 16.6112 |  |  |  |  |  |  |
|  | 1:11 | 1.4218 | 4.2559 | 14.8724 | 47.0202 | 42.7643 | 85.5286 | 14.4714 | 1.00 | 5.91 |
|  |  | 1.4169 |  | 15.5366 |  |  |  |  |  |  |
|  |  | 1.4257 |  | 17.1628 |  |  |  |  |  |  |
|  | 1:7 | 1.4181 | 4.2383 | 15.3169 | 46.3906 | 42.1523 | 84.3046 | 15.6954 | 1.00 | 5.37 |
|  |  | 1.3945 |  | 13.9109 |  |  |  |  |  |  |
|  |  | 1.4125 |  | 15.6628 |  |  |  |  |  |  |
| 7 M | $1: 9$ | 1.4234 | 4.2348 | 14.2597 | 46.5751 | 42.3403 | 84.6806 | 15.3194 | 1.00 | 5.53 |
|  |  | 1.3989 |  | 16.6526 |  |  |  |  |  |  |
|  |  | 1.4129 |  | 14.6566 |  |  |  |  |  |  |
|  | 1:11 | 1.4215 | 4.2521 | 17.5351 | 47.6556 | 43.4035 | 86.8070 | 13.1930 | 1.00 | 6.58 |
|  |  | 1.4177 |  | 15.4639 |  |  |  |  |  |  |
|  |  | 1.4348 |  | 16.7213 |  |  |  |  |  |  |
|  | 1:7 | 1.4513 | 4.3282 | 17.2703 | 46.5745 | 42.2463 | 84.4926 | 15.5074 | 1.00 | 5.45 |
|  |  | 1.4421 |  | 12.5829 |  |  |  |  |  |  |


| 6 M | 1:9 | 1.4235 | 4.2828 | 17.4417 | 46.6983 | 42.4155 | 84.8310 | 15.1690 | 1.00 | 5.59 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1.4315 |  | 13.3407 |  |  |  |  |  |  |
|  |  | 1.4278 |  | 15.9159 |  |  |  |  |  |  |
|  | 1:11 | 1.4329 | 4.3008 | 14.4466 | 47.7285 | 43.4277 | 86.8554 | 13.1446 | 1.00 | 6.61 |
|  |  | 1.4315 |  | 17.4385 |  |  |  |  |  |  |
|  |  | 1.4364 |  | 15.8434 |  |  |  |  |  |  |
| 5 M | 1:7 | 1.4259 | 4.2633 | 14.4075 | 46.5640 | 42.3007 | 84.6014 | 15.3986 | 1.00 | 5.49 |
|  |  | 1.4118 |  | 15.1644 |  |  |  |  |  |  |
|  |  | 1.4256 |  | 16.9921 |  |  |  |  |  |  |
|  |  | 1.4322 |  | 14.8323 |  |  |  |  |  |  |
|  | 1:9 | 1.4378 | 4.2999 | 17.8119 | 46.7454 | 42.4455 | 84.8910 | 15.1090 | 1.00 | 5.62 |
|  |  | 1.4299 |  | 14.1012 |  |  |  |  |  |  |
|  |  | 1.4246 |  | 18.1537 |  |  |  |  |  |  |
|  | 1:11 | 1.4198 | 4.2546 | 12.9906 | 47.7460 | 43.4914 | 86.9828 | 13.0172 | 1.00 | 6.68 |
|  |  | 1.4102 |  | 16.6017 |  |  |  |  |  |  |

Table 8. Determination of cement sand proportion based on lime 265 (standard cement-sand proportion used 1: 6)

| HCl molarity | HCl <br> dilution | Identification mark of platinum crucible | Weight of platinum crucible(g) | Weight of platinum crucible and residue (g) | Weight of residue (g) | \%age of Lime |  | \%age <br> of sand | Mix ratio result (by weight) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | cement | sand |
| 11 M | 1:7 | 1 | 42.9725 | 43.2162 | 0.2437 | 9.7480 | 14.9509 | 85.0491 | 1.00 | 5.69 |
|  | 1:9 | 2 | 43.8748 | 44.1078 | 0.233 | 9.3200 | 14.2945 | 85.7055 | 1.00 | 6.00 |
|  | 1:11 | 3 | 41.5668 | 41.7861 | 0.2193 | 8.7720 | 13.4540 | 86.5460 | 1.00 | 6.43 |
| 10 M | 1:7 | 4 | 44.6616 | 44.8877 | 0.2261 | 9.0440 | 13.8712 | 86.1288 | 1.00 | 6.21 |
|  | 1:9 | 5 | 40.4581 | 40.6789 | 0.2208 | 8.8320 | 13.5460 | 86.4540 | 1.00 | 6.38 |
|  | 1:11 | 6 | 37.7160 | 37.9236 | 0.2076 | 8.3040 | 12.7362 | 87.2638 | 1.00 | 6.85 |
| 9 M | 1:7 | 7 | 43.4475 | 43.6603 | 0.2128 | 8.5120 | 13.0552 | 86.9448 | 1.00 | 6.66 |
|  | 1:9 | 8 | 44.9812 | 45.1902 | 0.209 | 8.3600 | 12.8221 | 87.1779 | 1.00 | 6.80 |
|  | 1:11 | 9 | 23.6816 | 23.8829 | 0.2013 | 8.0520 | 12.3497 | 87.6503 | 1.00 | 7.10 |
| 8 M | 1:7 | 10 | 41.7885 | 41.9876 | 0.1991 | 7.9640 | 12.2147 | 87.7853 | 1.00 | 7.19 |
|  | 1:9 | 11 | 26.5279 | 26.7194 | 0.1915 | 7.6600 | 11.7485 | 88.2515 | 1.00 | 7.51 |
|  | 1:11 | 12 | 68.9154 | 69.1025 | 0.1871 | 7.4840 | 11.4785 | 88.5215 | 1.00 | 7.71 |
| 7 M | 1:7 | 1 | 42.9724 | 43.1692 | 0.1968 | 7.8720 | 12.0736 | 87.9264 | 1.00 | 7.28 |
|  | 1:9 | 2 | 43.8745 | 44.0645 | 0.1900 | 7.6000 | 11.6564 | 88.3436 | 1.00 | 7.58 |
|  | 1:11 | 3 | 41.5668 | 41.7529 | 0.1861 | 7.4440 | 11.4172 | 88.5828 | 1.00 | 7.76 |
| 6 M | 1:7 | 4 | 44.6613 | 44.8578 | 0.1965 | 7.8600 | 12.0552 | 87.9448 | 1.00 | 7.30 |
|  | 1:9 | 5 | 40.4579 | 40.6479 | 0.19 | 7.6000 | 11.6564 | 88.3436 | 1.00 | 7.58 |
|  | 1:11 | 6 | 37.7158 | 37.9004 | 0.1846 | 7.3840 | 11.3252 | 88.6748 | 1.00 | 7.83 |
| 5 M | 1:7 | 7 | 43.4474 | 43.6419 | 0.1945 | 7.7800 | 11.9325 | 88.0675 | 1.00 | 7.38 |
|  | 1:9 | 8 | 44.9809 | 45.1707 | 0.1898 | 7.5920 | 11.6442 | 88.3558 | 1.00 | 7.59 |
|  | 1:11 | 9 | 23.6815 | 23.8651 | 0.1836 | 7.3440 | 11.2638 | 88.7362 | 1.00 | 7.88 |

## Conclusion

The purpose of this study is to verify the accuracy of cement-sand mix ratio analysis in cement mortar. It provides complete awareness about the percentage values of insoluble residues and calcium oxide variation by changing the standard ratio and concentration of the hydrochloric acid solution. The increasing dilution of
the HCl solution has proved ineffective in the proper de-composition of hydrates of cement. Therefore, the cement contents do not dissolve completely in the solution and deviated results are achieved. The reactivity order of molarities of HCl solutions to their ratios is $1: 7>1: 9>1: 11$ for all molarities. It is concluded that using $11 \mathrm{M}(1: 9) \mathrm{HCl}$ solution confirms the standard
ratios. Hence, the determination of the cement-sand ratio on a lime basis is recommended only under the standard solution condition $11 \mathrm{M}(1: 9)$. It is pertinent to mention here that a false common practice in the field is used to estimate the cement sand proportion of mortar samples based on insoluble residue using unstandardized HCl . The present study not only provide the importance of Test Method BS 4550: 1970 but also provide awareness to the field chemists working in civil departmental laboratories that do not estimate cement sand proportion in mortar based on insoluble residue results.

Conflict of Interest. The authors declare no conflict of interest.

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